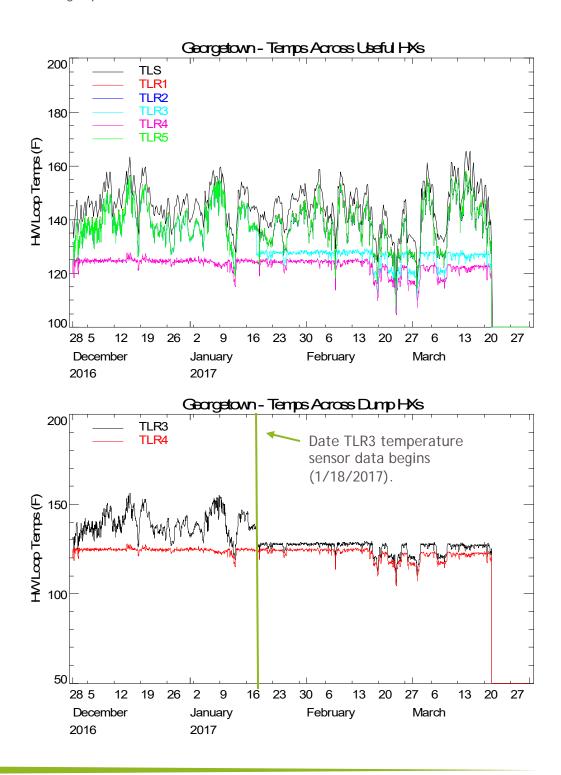
CDH was on site on January 18, 2017. The purpose of this visit was to determine the cause of low flow measurements. While on site the TLR3 temperature sensor, which was never wired, was found and wired. As of 1/18/2017 TLR3 is no longer stipulated as being equal to TLR2.



While on site the FL1 flow was verified using a Portaflow portable ultrasonic flow meter. The table below shows the Portaflow readings as compared to the readings on the Obvius from the installed Onicon FL1 flow meter.

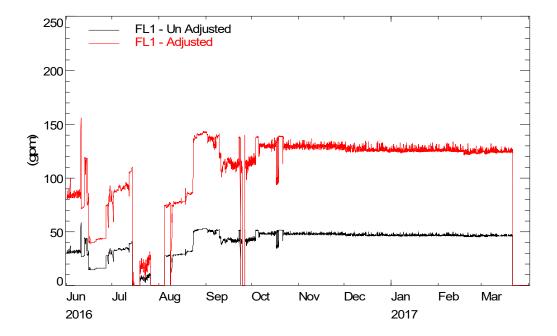
Obvius Reading (gpm)	Dortaflow Poading	anml
Obvius Neauling (gpill)	ruitanuw neaunig (	gpiiij

	1 01 tall 0 11 11 tala 111 10 (8pm)
88.0	127.4
88.6	126.8
89.9	127.0
87.0	126.3
87.5	126.9

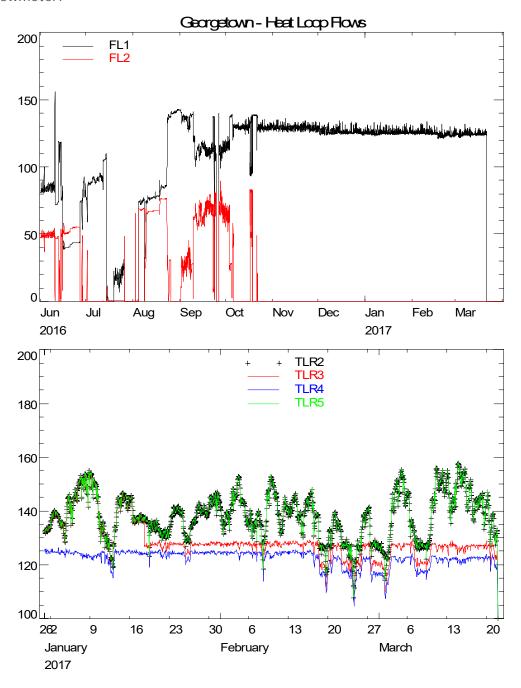
Avg: 88.2 126.9

When the flow meter was last pulled from the pipe to be sent back to Onicon to be respanned, it was observed that the turbine and parts inserted into the flow were covered with a black oily substance. It is suspected that the difference in flow measurements in the table above is due to fouling of the meter, caused by the oil present in the heat recovery loop. To correct for this, the Onicon readings are being multiplied by the ratio of the observed flows. This correction is applied to the measured data in addition to correcting for the re-spanning of the flow meter which was changed from 0 - 80 gpm to 0 - 150 gpm.

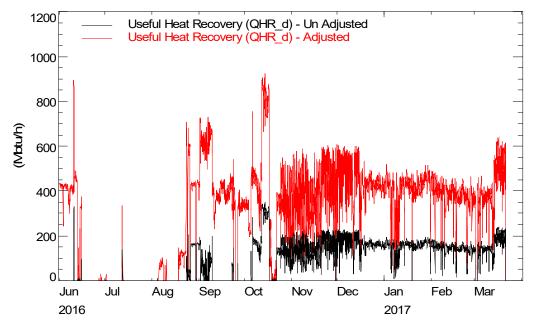
$$FL1_{corrected} = FL1 * \begin{bmatrix} 150 / \\ 80 \end{bmatrix} * \begin{bmatrix} 126.9 / \\ 88.2 \end{bmatrix}$$



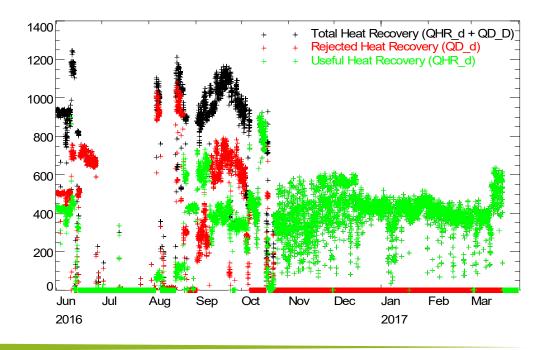
While on site FL2 was not verified due to the fact that there is no flow thru the dump radiator. We are confident that there is in fact no flow and that the FL2 flow meter is not working due to the recovered heat loop temperatures (since TLR3 was wired). The fact that TLR2 and TLR5 temperature measurements are identical, and TLR3 and TLR4 are much lower, indicates that flow is bypassing the dump radiator loop and FL2 flowmeter.



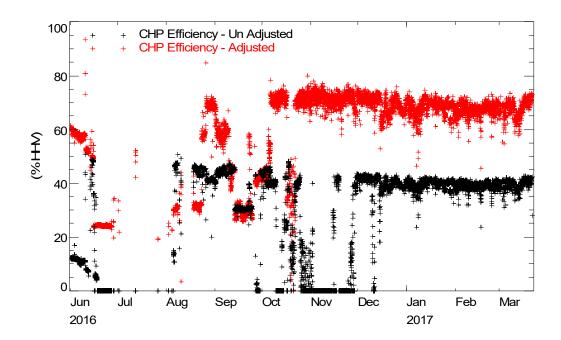
Adjusting the FL1 flow had a considerable effect on the heat recovery, effectively raising it by a factor of 2.7. The adjusted heat recovery values are still well within the engine ratings of 700 Mbtu/h from each engine or 1,400 Mbtu/hr for the system.

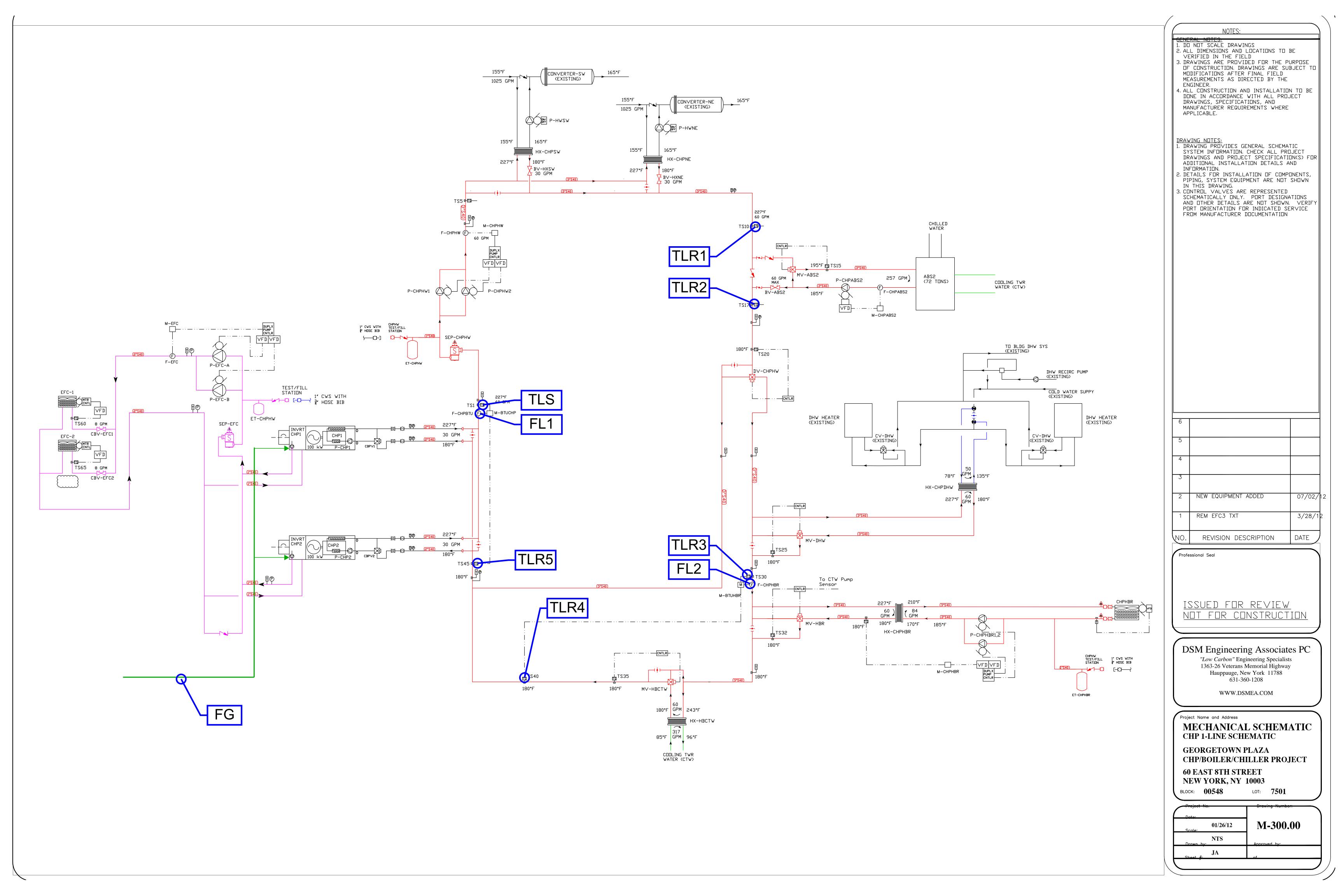


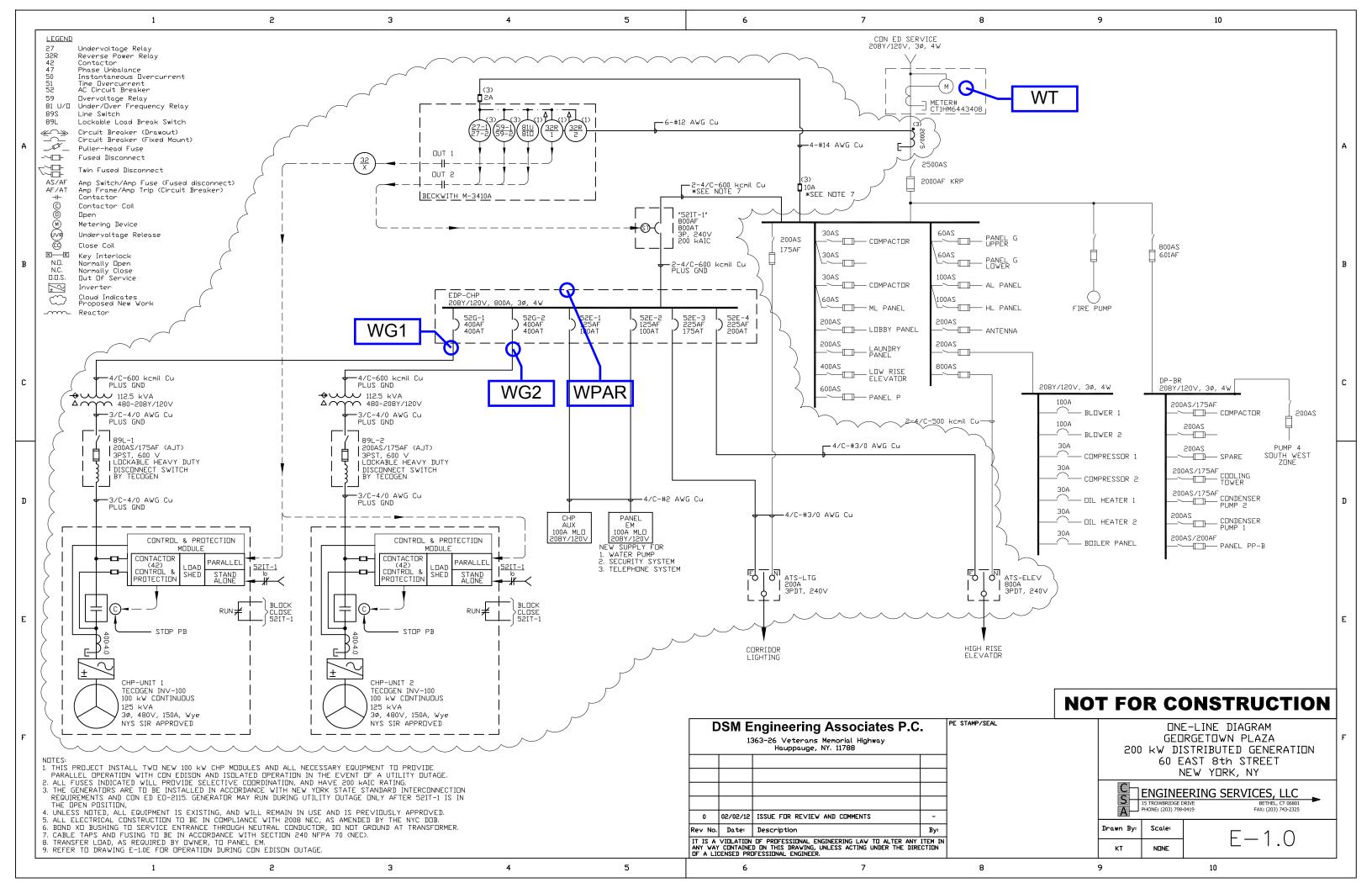
Previously, while stipulating TLR3 = TLR2, the calculated rejected heat was being artificially elevated. This is because useful heat recovered for DHW heating via HX-CHPDHW was being counted as rejected heat. When the FL2 loop bypass began in October 2016, all rejected heat recovery went to zero, so this was no longer an issue. Now that TLR3 is being properly measured the rejected heat recovery will be accurately calculated when heat is being rejected.



Adjusting the flow had a significant impact on the measured CHP efficiency. The collected data now is accurately reflecting the observed, on site, system performance and is in line with the INV-100 CHP efficiency rating of 82.4% HHV.









## Features & Benefits

- 100 kW Continuous/125 kW Peaking
- Standardized Interconnection
- Black-Start Grid-Independent Operation
- Microgrid compatible with licensed CERTS<sup>1</sup> power balancing control software
- Premium Quality Wave Form, Voltage and Power Factor for Special Applications (e.g. computer server farms or precision instrumentation)
- Power Boost for Demand-Side Response
- Enhanced Efficiency from Variable Speed Operation
- Simplified Inter-Unit Controls for either Mode of Operation (parallel or standby)
- ETL Listed Labeled for compliance with UL 1741 Utility Interactive; Inverters, Converters, Controllers and Interconnection System Equipment for Use with Distributed Energy Resources
- Renewable Energy Compatible, a Clean Energy Solution for Today and Tomorrow

  'CERTS Consortium for Electric Reliability Technology Solutions





## **TECOGEN, Inc.**

- Over 25 years experience in packaged cogeneration, chillers and refrigeration systems
- More than 1,400 operating units in the field
- Extensive service network with factory-trained technicians exclusively servicing Tecogen products

## Specifications: 1

Engine	Proven Low-Emission Natural Gas V-8 Engine, 454 cid, 1000-3000 rpm	
Generator	Water-Cooled Permanent Magnet Generator	
Inverter	Customized Power Electronics with Patented Topology for Variable Speed and Standby Operation	
Controls	ontrols  TecoNet <sup>™</sup> Microprocessor-Based System, Fully Automatic, Fault Monitoring, Lead/Lag Multiple Unit Control, Modbus Networking & Remote Telecommunications	

Electric Output	100 kW Continuous / 125 kW Peaking <sup>2</sup>	
	480 VAC / 3 PH / 60 Hz	
Standalone Electric Capacity	I25 kVA	
Thermal Output		
Engine	700,000 Btu/hr @ 230°F Max	
Generator/Power Electronics	27,000 Btu/hr @ I29°F Max	
Electric Efficiency		
@ LHV of 905 Btu/scf	30.4%	
@ HHV of 1020 Btu/scf	27.0%	
System Efficiency <sup>3</sup>		
@ LHV of 905 Btu/scf	92.9%	
@ HHV of 1020 Btu/scf	82.4%	
Gas Input	I 238 scfh	
	1625 scfh Peaking	
Required Gas Pressure	10-28" wc	
Hot Water	30 gpm	
Maximum Leaving Water Temperature	230 °F	
Maximum Entering Water Temperature	180 °	
Air Emissions <sup>5</sup>		
• NOx	I.5 lb/MWh	
• CO	2.0 lb/MWh	
• VOC	I.0 lb/MWh	
Weight	3,850 lb	
Dimensions	7'4"L x 4'W x 5'.9" H	
ETL Listed - Labeled for compliance with UL 1741 - Utility Interactive; Inverters, Converters,		

Controllers and Interconnection System Equipment for Use with Distributed Energy Resources

- 1. All specifications are +/- 5% and are subject to change without notice.
- 2. Peaking capacity is available for 100 hours per year only when grid connected.
- 3. Includes engine heat recovery only (not generator/power electronics heat).
- 4. Above performance data is valid up to 104 °F ambient temperature
- 5. Lower emissions options are available with the use of additional catalyst material.

